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The reality of the administrative at communication Al Quds University from the employees' point of view

Abstract

This study aimed at exploring the reality of the administrative at communication Al Quds University from the employees' point of view, and the effect of the study's variables: sex, educational qualification, and years of experience, age group and the nature of work on this. the study's community consisted of all the employees of Al Quds University, numbering 1117 employees (personnel affairs department, Al Quds University, 2010). A random clustered sample was used in distributing the questionnaires. The sample consisted of three clusters: the administrators, the academics, and the services with a percentage of 11.7%.

Consequently, the questionnaire was selected as a tool for collecting the data relating to the study subject. The data were presented to a groub of arbitrators to examine the extent to which data are credible. The date was statistically processed by extracting the arithmetic means and standard deviations for each paragraph in the questionnaire.

To realize the Constance of the questionnaire, the total grade of Constance coefficient of the study standard was calculated in accordance with the Constance formula of Cronpach Alpha. The total grade was (0.9661). This result indicates that this tool enjoys a Constance which fulfils the purposes of the study.

The study was concluded with a group of results, the most important of which are the following: The results of the study on the reality of the administrative communication at Al Quds University showed that it attained a medium arithmetic mean gained through the answers of the objects of the study sample.

The study was concluded with a group of recommendations, the most important of which are the following: To take the necessary procedures which reduce dependence on the conventional means used in communication, and to benefit from innovations and methods in communication that effectively contribute to rapid transfer of modern information, such as the interner.

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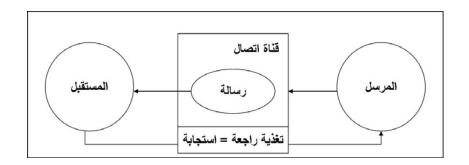
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23.9	28	5
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0.89	3.68		1
0.87	3.54		2
0.99	3.62	·	3
1.03	3.15		4
0.97	3.21	·	5
1.06	3.28	·	6
1.07	2.86		7
0.99	3.63		8
1.07	3.02		9
0.89	3.67		10
0.57	3.37		•

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0.866	3.79		1
0.950	3.73	·	2
0.930	3.70		3
0.956	3.70		4
0.894	3.44		5
0.71	3.68		•

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0.911	3.74		1
0.960	3.69		2
0.870	3.66		3
0.946	3.60	·	4
0.74	3.68		

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0.936	3.38		1
0.970	3.31	·	2
0.949	3.29	·	3
0.902	3.29	·	4
0.882	3.07	·	5
0.79	3.28		

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0.971	3.62	1
0.948	3.58	2
0.98	3.56	3
0.970	3.49	4
0.896	3.47	5
0.83	3.55	

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0.71	3.68	1
0.74	3.68	2
0.79	3.49	3
0.83	3.55	4
0.76	3.60	

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0.870 3.66 1 2 0.864 3.57 3 0.932 3.55 4 0.924 3.47 5 0.931 3.42 0.79 3.54

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0.812	3.64		1
0.844	3.56		2
0.866	3.53		3
0.970	3.50		4
0.961	3.49		5
0.836	3.47	·	6
0.960	3.46		7
0.72	3.53		

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0.761 3.72 1 2 0.785 3.67 3 0.869 3.61 0.803 3.45 4 0.832 3.28 5 0.68 3.55

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0.792 3.43 1 0.896 3.52 2 3 3.43 0.864 3.35 4 0.865 3.27 5 0.847 0.71 3.41

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0.905	3.53	1
0.886	3.52	2
0.857	3.51	3
0.867	3.50	4
0.919	3.33	5
0.77	3.48	

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0.79	3.54	1
0.72	3.53	2
0.68	3.55	3
0.71	3.41	4
0.77	3.48	5
0.73	3.50	

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1.029	3.30		1
1.018	3.22		2
1.009	3.22	.(3
0.955	3.18		4
0.987	3.17	·	5
0.997	3.06	·	6
1.011	3.05	·	7
1.023	2.93	·	8
0.75	3.15		

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0.994	3.95	.()	1
0.961	3.91	·	2
1.004	3.91		3
1.018	3.88		4
0.973	3.83	·	5
0.983	3.74	.()	6
1.108	3.64	·	7
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 $(0.05 \ge \alpha)$

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 $(0.05 \geq \alpha)$

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	"t"				
0.091	1.702	0.64640	3.5617	81	
		0.50080	3.3552	36	

(0.091) (1.702) () (0.05 $\geq \alpha$)

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 $(0.05 \geq \alpha)$

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0.910	0.248	0.095	4	0.381	
		0.383	112	42.888	
			116	43.268	

(16.4) (one way ANOVA)

(0.910) (0.248)) $(0.05 \ge \alpha)$

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0.910	0.248	0.095	4	0.381	
		0.383	112	42.888	
			116	43.268	

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 $(0.05 \ge \alpha)$

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0.00000	3.9286	2	
0.60884	4.0026	7	
0.62515	3.7366	4	
0.49262	3.3591	27	
0	3.1786	1	
0.62730	3.5804	36	
0.64243	3.3924	40	

18.4

.(19.4) (one way ANOVA)

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	11 11				
0.125	1.711	0.616	6	3.693	
		0.360	110	39.575	
			116	43.268	

(0.125) (1.711) $(0.05 \ge \alpha)$

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 $(0.05 \ge \alpha)$

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0.65262	3.6320	28	5	
0.47101	3.3482	34	10-6	
0.66572	3.4348	20	15-11	
0.67357	3.6202	15	20-16	
0.65190	3.5375	20	20	

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.(19.4) (one way ANOVA)

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		0.400	4	1.601	
0.372	1.076	0.372	112	41.667	
			116	43.268	

(0.372) (1.076) $(0.05 \ge \alpha)$

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 $(0.05 \ge \alpha)$

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0.64751	3.4300	61	
0.54504	3.5111	45	
0.59913	3.8231	11	

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(one way ANOVA)

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0.143	1.979	0.726	2	1.452	
		0.367	114	41.816	
			116	43.268	

(0.143) (1.979) $(0.05 \ge \alpha)$

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 $(0.05 \geq \alpha)$

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	"t"				
0.010	2.415	0.54500	3.4531	81	
0.019	2.415	0.58767	3.1750	36	
0.061	0.047	0.77568	3.6790	81	
0.961	0.047	0.56194	3.6722	36	
0.227	1 100	0.77739	3.7315	81	
0.237	1.188	0.64396	3.5556	36	
0.100		0.85173	3.3407	81	
0.180	1.349	0.61811	3.1278	36	
0.024	2 200	0.85278	3.6568	81	
0.024	2.298	0.71950	3.3056	36	
		0.80740	3.6099	81	
0.151	1.444	0.72408	3.3833	36	
		0.73879	3.5608	81	
0.455	0.749	0.68597	3.4524	36	
		0.71141	3.6963	81	
0.130	1.526	0.59607	3.4889	36	
0.054		0.75299	3.4889	81	
0.061	1.895	0.57127	3.2222	36	
0.01.5	1.0.1-	0.82839	3.5432	81	
0.215	1.247	0.62951	3.3500	36	
0.001	4.505	0.64640	3.5617	81	
0.091	1.702	0.50080	3.3552	36	

 $(0.05 \ge \alpha)$

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					<u> </u>
0.67401	3.1000	8	25		
0.59204	3.2975	40		-25	
0.50405	3.4744	39	36		_
0.67011	3.3800	20	46	-36	
				-46	
0.40770	3.4200	10	55		
1.13011	3.4500	8	25		
0.66069	3.7200	40	36	-25	
0.59176	3.7333	39	46	-36	
0.79313	3.6800	20	55	-46	
0.87458	3.4600	10	55		
1.03887	3.5313	8	25		
0.71832	3.6813	40	36	-25	
0.60258	3.7692	39	46	-36	
0.91802	3.6750	20	55	-46	
0.74582	3.4250	10	55		
1.01278	3.3500	8	25		
0.74255	3.1800	40	36	-25	
0.83140	3.3333	39	46	-36	
0.80812	3.2600	20	55	-46	
0.70553	3.4000	10	55		
1.03095	3.4000	8	25		
0.76713	3.5150	40	36	-25	
0.79411	3.5692	39	46	-36	
0.88234	3.7800	20	55	-46	
0.94775	3.2600	10	55		

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0.92852	3.4250		8		25	
0.73861	3.4900	40		26		
0.75665	3.6103	39		36 46	-25	
0.98280	3.5200	20			-36 -46	
0.65997	3.6000	10		55		_
0.87544	3.4464		8		25	
0.76466	3.5179	40		36	-25	
0.61630	3.6264	39		46	-36	
0.75607	3.4714	20			-46	
0.82822	3.3571	10		55		
0.90356	3.4250		8		25	
0.65781	3.6100	40		36	-25	_
0.57651	3.7026	39		46	-36	_
0.79498	3.7400	20			-46	_
0.77746	3.4000	10		55		
0.87137	3.3750		8	25		
0.57054	3.4750	40		36	-25	
0.67662	3.4462	39		46	-36	
0.91185	3.1900	20		55	-46	
0.82624	3.4400	10		55		
0.87137	3.3750		8		25	
0.57054	3.4750	40		36	-25	
0.67662	3.4462	39		46	-36	
0.91185	3.1900	20		55	-46	
0.82624	3.4400	10		55		
0.93465	3.4250		8		25	
0.75949	3.5600	40		36	-25	
0.69239	3.4513	39		46	-36	
0.93223	3.4800	20		55	-46	7
0.80994	3.3600	10		55		
0.86760	3.3661		8		25	
0.54808	3.4835	40		36	-25	
0.56669	3.5614	39		46	-36	
0.71432	3.5009	20		55	-46	
0.66709	3.4107	10		55		

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. . 4 0.311 1.244 0.326 112 36.532 0.954 0.436 37.777 116 0.270 4 1.081 0.721 0.521 0.519 112 58.107 116 59.188 0.284 4 1.138 112 0.558 62,495 0.729 0.510 116 63.632 4 0.175 0.699 0.895 0.273 0.641 112 71.839 116 72.538 4 2.142 0.536 0.543 0.777 0.690 112 77.230 116 79.372 4 0.111 0.442 0.952 0.174 0.637 112 71.339 71.781 116 0.198 4 0.791 0.829 0.371 0.532 112 59.636 116 60.427 4 0.332 1.328 0.590 0.7060.470 112 52.669 116 53.997 0.301 4 1.206 112 57.349 0.589 0.672 0.512 116 58.555 0.114 4 0.455 112 69.244 0.946 0.184 0.618 116 69.699

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0.07071	3.6500	2	
0.58023	3.8000	7	
0.68313	3.5000	4	
0.46596	3.1407	27	
	2.9000	1	
0.61202	3.4028	36	
0.56318	3.3975	40	
0.00000	4.0000	2	
0.83038	4.0571	7	
0.57446	4.0500	4	
0.71452	3.5852	27	
	3.6000	1	
0.67912	3.7778	36	
0.74082	3.5300	40	
0.35355	4.2500	2	
0.76959	4.2143	7	
0.52042	3.8750	4	
0.79034	3.5185	27	
	3.7500	1	
0.68646	3.7639	36	
0.75267	3.5625	40	

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0.14142	3.7000	2		
0.76966	3.7714	7		
0.86987	3.4500	4		
0.65564	3.2296	27		
	2.4000	1		
0.78903	3.2833	36		
0.88345	3.1950	40		
0.00000	4.0000	2		
0.58716	4.3143	7		
0.83865	3.8500	4		
0.67567	3.3037	27		
	3.0000	1		
0.84903	3.6500	36		
0.88492	3.4500	40		
0.14142	4.1000	2		
0.73679	4.0571	7		
0.73711	3.9500	4		
0.68687	3.3778	27		
	3.0000	1		
0.77310	3.7056	36		
0.83450	3.3550	40		
0.20203	4.1429	2		
0.81411	3.8367	7		
0.75930	3.8214	4		
0.63879	3.4392	27		
	3.4286	1		
0.81374	3.6151	36		
0.67820	3.3964	40		

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0.538 6 3.227	
0.125 1.712 110 34.550	
0.314 116 37.777	
0.540 6 3.240	
0.390 1.062 110 55.947	
0.509 116 59.188	
0.248 1.333 0.719 6 4.314	
110 59.319	
0.539 116 63.632	
0.548 6 3.289	
0.519 0.871 110 69.250	
0.630 116 72.538	
1.259 6 7.554	
0.082 1.928 110 71.818	
0.653 116 79.372	
1.088 6 6.529	
0.099 1.835 110 65.252	
0.593 116 71.781	
0.493 6 2.956	
0.467 0.943 110 57.471	
0.522 116 60.427	
0.747 6 4.483	
0.138 1.660 110 49.513	
116 53.997	
0.090 1.882 0.909 6 5.451	
1111011 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
0.090 1.882 110 53.103	

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	11 11				
0.202		0.724	6	4.342	
0.302	1.218	0.504	110	65.357	
		0.594	116	69.699	
0.125	1 711	0.616	6	3.693	
0.125	1.711	0.260	110	39.575	
		0.360	116	43.268	

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0.70021	2 2	• •		
0.58031	3.3750	28	5	
0.53244	3.2882	34	10-6	
0.62568	3.3100	20	15-11	
0.65005	3.4400	15	20-16	
0.52763	3.4950	20	20	
0.81624	3.8571	28	5	
0.50509	3.5059	34	10-6	
0.86542	3.6500	20	15-11	
0.78364	3.7867	15	20-16	
0.64269	3.6600	20	20	
0.84020	3.8661	28	5	
0.67832	3.5441	34	10-6	
0.73840	3.5625	20	15-11	
0.65101	3.9333	15	20-16	
0.72491	3.5625	20	20	
0.84977	3.4286	28	5	
0.66673	3.2176	34	10-6	
0.89537	2.9200	20	15-11	
0.84177	3.4000	15	20-16	
0.69857	3.4200	20	20	
0.79506	3.6786	28	5	
0.66469	3.3000	34	10-6	
0.94568	3.5200	20	15-11	
0.84470	3.8267	15	20-16	
0.94362	3.6100	20	20	

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0.75687	3.6214	28	_	
		34	5	
0.68456	3.3471		10-6	
0.92110	3.5000	20	15-11	
0.82393	3.7200	15	20-16	
0.82615	3.6600	20	20	
0.70615	3.7551	28	5	
0.66056	3.2563	34	10-6	
0.73635	3.5143	20	15-11	
0.71836	3.7143	15	20-16	
0.74534	3.5429	20	20	
0.73001	3.7429	28	5	
0.57571	3.4647	34	10-6	
0.69668	3.6700	20	15-11	
0.62183	3.7333	15	20-16	
0.81273	3.6500	20	20	
0.70102	3.5429	28	5	
0.62131	3.3059	34	10-6	
0.70450	3.3500	20	15-11	
0.85590	3.3600	15	20-16	
0.78780	3.4800	20	20	
0.79904	3.7071	28	5	
0.61089	3.3882	34	10-6	
0.87365	3.4700	20	15-11	
0.91298	3.4933	15	20-16	
0.78967	3.3400	20	20	
0.65262	3.6320	28	5	
0.47101	3.3482	34	10-6	
0.66572	3.4348	20	15-11	
0.67357	3.6202	15	20-16	
0.65190	3.5375	20	20	

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		0.171	4	0.685					
0.723	0.517	0.171	112	37.091	<u> </u>				
	0.517	0.331	116	37.091	1				
		0.526	4						
0.394	1.033	0.526		2.105	1				
		0.510	112	57.083	<u> </u>				
			116	59.188					
0.226	1.439	0.778	4	3.111	-				
0.220	1.137	0.540	112	60.521	_				
			116	63.632					
0.176	1.611	0.987	4	3.948					
0.170	1.011	0.612	112	68.591					
		0.012	116	72.538					
0.233	1.418	0.956	4	3.826					
0.233	1.416	1.410	1.410	1.410	1.418	0.675	112	75.546	
		0.675	116	79.372					
0.461	0.000	0.564	4	2.257					
0.461	0.909	0.721	112	69.524					
		0.621	116	71.781					
0.060	2 2 4 4	1.121	4	4.483					
0.069	2.244	0.500	112	55.944	1				
		0.500	116	60.427					
0.522	0.505	0.371	4	1.485					
0.533	0.792	0.150	112	52.512					
		0.469	116	53.997	1				
:		0.267	4	1.069					
0.721	0.521		112	57.485					
		0.513	116	58.555	-				
			110	36.333					

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0 4 5 0		0.531	4	2.126	
0.478	0.881	0.602	112	67.573	
		0.603	116	69.699	
0.252	1.076	0.400	4	1.601	
0.372	1.076	0.372	112	41.667	
			116	43.268	

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0.55106	2 2 7 7 1		_	
0.55186	3.3754	61		
0.59618	3.2844	45		
0.50847	3.6636	11		
0.77984	3.5574	61		
0.59669	3.7822	45		
0.71198	3.9091	11		
0.80140	3.5984	61		
0.62679	3.7056	45		
0.79057	4.0000	11		
0.83629	3.2623	61		
0.73038	3.2133	45		
0.75895	3.6000	11		
0.83855	3.4820	61		
0.81352	3.5333	45		
0.75607	3.9818	11		
0.80755	3.4230	61		
0.75657	3.6178	45		
0.71706	3.8727	11		
0.73379	3.4543	61		
0.69613	3.5810	45		
0.77196	3.7143	11		

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0.72889	3.5148	61	
0.59939	3.7067	45	
0.62260	3.9818	11	
0.76858	3.2721	61	
0.58872	3.4978	45	
0.69544	3.7818	11	
0.84366	3.4393	61	
0.67635	3.4267	45	
0.63761	3.9636	11	
0.64751	3.4300	61	
0.54504	3.5111	45	
0.59913	3.8231	11	

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		T	1	1	T	1									
			_												
0.140	1.997	0.639	2	1.279											
0.140	1.997	0.320	114	36.498											
			116	37.777											
0.146	1.056	0.982	2	1.964											
0.146	1.956	0.502	114	57.224		1									
			116	59.188											
		0.781	2	1.562											
0.243	1.434		114	62.071		-									
		0.544	116	63.632		-									
		0.671	2	1.343											
0.345	1.075	1.075	1.075	1.075	1.075	1.075	1.075	1.075	1.075	1.075		114	71.195		-
		0.625	116	72.538											
	1.736	1 = 2 6	1.173	2	2.346										
0.181			114	77.027											
		0.676	116	79.372											
	1.909	1.163	2	2.326											
0.153		1.909	1.909	1.909	1.909	1.909	1.909	1.909	1.909		114	69.455		-	
		0.609	116	71.781		-									
		0.419	2	0.839											
0.451	0.802		114	59.588		1									
		0.523	116	60.427		1									
		1.218	2	2.435											
0.072	2.692		114	51.561		1									
		0.452	116	53.997		1									
		1.513	2	3.026											
0.052	3.106		114	55.529		1									
		0.487	116	58.555		1									
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	11 11				
		1.400	2	2.800	
0.097	2.386				
0.077	2.300		114	66.899	
		0.587			
			116	69.699	
			_		
		0.726	2	1.452	
0.143	1.979				
0,12,10			114	41.816	
		0.367			
		0.207	116	43.268	

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68	 2.3
69	 3.3
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35		6.3
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40		2.4
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41		4.4
42		5.4
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42		6.4
43		7.4
15		7.1
44		8.4
77		0.4
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